

Coupled Fluid-Flow/Mechanical/Fracture Simulations of Hydraulic Fracture Propagation

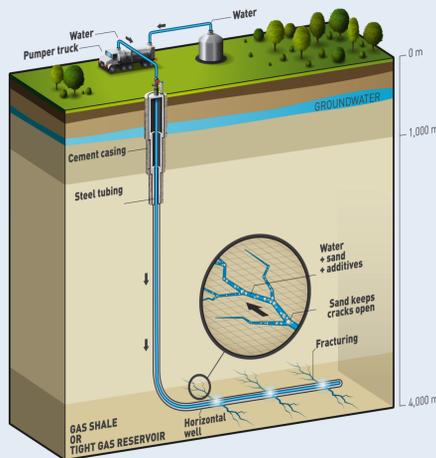
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Introduction

Hydraulic fracturing is the propagation of fractures in a rock layer, as a result of the action of a pressurized fluid. It is the technique of choice for enhancing permeability in reservoirs for extraction of petroleum, natural gases etc.

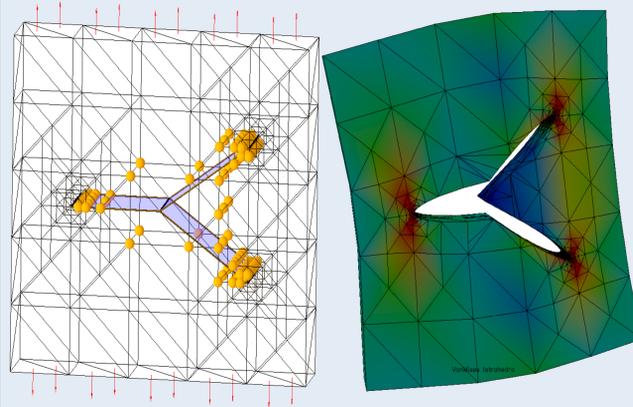


Objectives

- Fully coupled formulation for non-planar three dimensional hydraulic fracturing
- Coupling for fracture propagation criterion with mechanical deformation and fluid-flow in the fracture
- Computationally efficient techniques for time marching of the solution

Generalized FEM

- GFEM can be interpreted as FEM with shape functions built using concept of Partition of Unity
- GFEM shape function = FEM shape fn * enrichment



Salient Features

- Discontinuity and singularity along the crack front modeled via enrichment functions. No need for fracture mesh to conform to crack surfaces
- Fracture surface represented explicitly independent of volume mesh
- Adaptive volume mesh refinement along the crack front and crack surface

Coupled Hydro-Mechanical Formulation

Governing Equations for Porous Medium

$$\int_{\Omega} \nabla_s \delta u : \sigma(u) d\Omega = \int_{\partial\Omega} \bar{t} \cdot \delta u d\Gamma + \int_{\Gamma_c^+} \bar{t}_c^+ \cdot [\delta u] d\Gamma_c$$

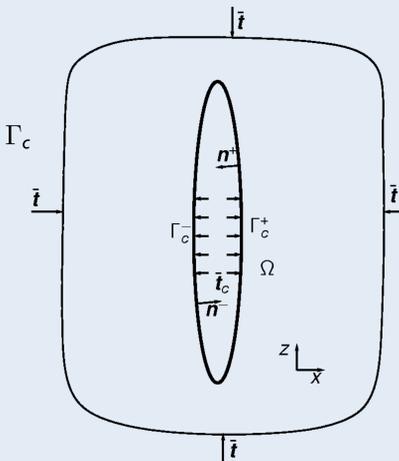
where $[\delta u]$ is the virtual displacement jump across the crack surface Γ_c

Governing Equations for Fluid-Flow in Fracture

$$\text{Reynold's Lubrication Equation: } \nabla_{\bar{x}} \cdot q + \frac{\partial w}{\partial t} = Q_I - Q_L$$

$$\text{Poiseuille's cubic law: } q = \frac{w^3}{12\mu} \nabla p$$

$$\int_{\Gamma_c} \frac{w^3}{12\mu} \nabla_{\bar{x}} \delta p \cdot \nabla_{\bar{x}} p d\Gamma_c = \int_{\Gamma_c} \delta p \left[Q_I - Q_L - \frac{\partial w}{\partial t} \right] d\Gamma_c + \int_{\partial\Gamma_c} \bar{q}(s) \delta p ds$$



Coupling Conditions

$$\bar{t}_c^+ = -pn^+$$

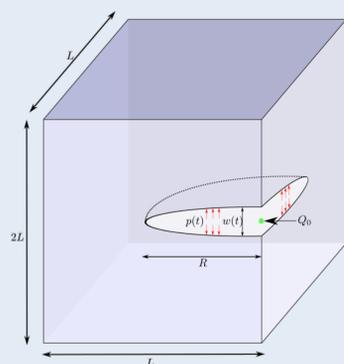
$$w = [[u]] \cdot n^-$$

System of Equations

$$\begin{bmatrix} K_u^{n+1} & -(K_c^{n+1})^T \\ K_c^{n+1} & \Delta t K_p^{n+1} \end{bmatrix} \begin{bmatrix} \hat{u}^{n+1} \\ \hat{p}^{n+1} \end{bmatrix} = \begin{bmatrix} (K_c^{n+1,n}) \hat{u}^n + \Delta t Q_p^{n+1} + \Delta t \bar{q}_p^{n+1} \end{bmatrix}$$

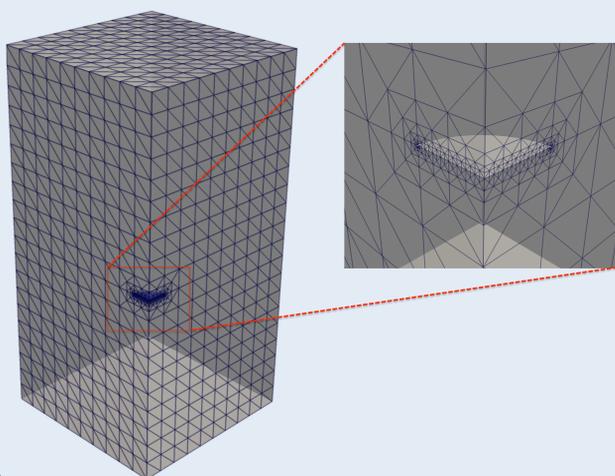
Verification Example

Planar Penny Shaped Fracture

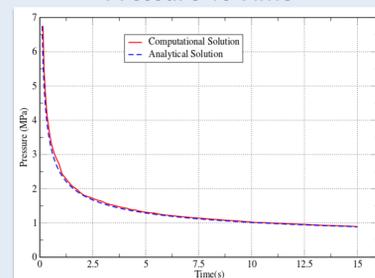


$L = 5\text{ m}$ $R = 0.5\text{ m}$
 Incomp. Newtonian fluid with viscosity
 $\mu = 0.1\text{ cPoise}$
 Injection rate at center of fracture
 $Q = 0.001\text{ m}^3/\text{s}$
 $E = 17\text{ GPa}$
 $\nu = 0.2$
 $K_{Ic} = 1.46\text{ MPa}\sqrt{\text{m}}$
 $\Delta a_{max} = 0.05\text{ m}$

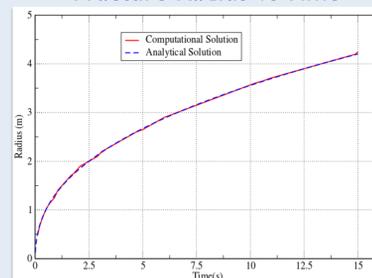
Input GFEM discretization and mesh refinement



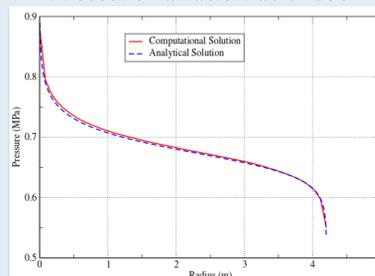
Pressure vs Time



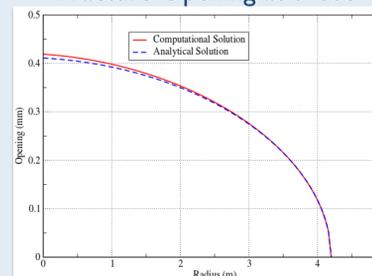
Fracture Radius vs Time



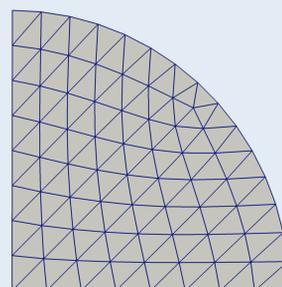
Pressure Variation at t=15s



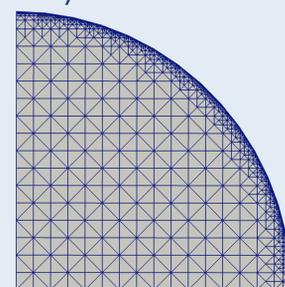
Fracture Opening at t=15s



Geometrical Crack Surface



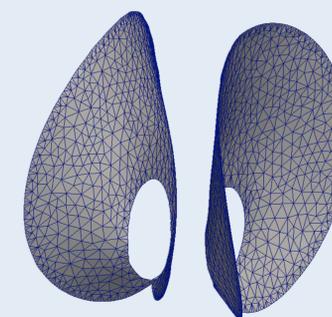
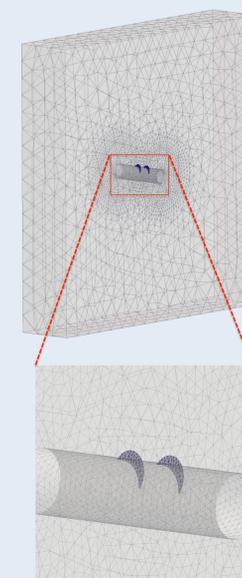
Automatically Generated Fluid Mesh



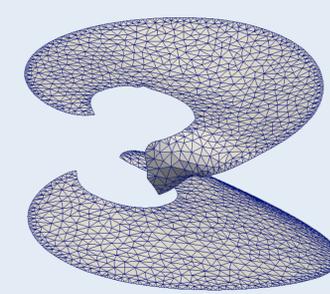
Fracture Interaction

$\sigma_h = \sigma_H = 1.0\text{ MPa}$ and $\sigma_v = 2.5\text{ MPa}$
 $E = 5\text{ GPa}$, $\nu = 0.2$ and $K_{Ic} = 0.1\text{ MPa}\sqrt{\text{m}}$
 Pressure applied, $p = 3.0\text{ MPa}$

Different Interaction Scenarios



$d = 0.2\text{ m}$
 $\text{Angle} = 0^\circ$



$d = 0.2\text{ m}$
 $\text{Angle} = 45^\circ$

Conclusions and References

Conclusions

- Novel formulation using a GFEM for coupling of solid deformation and fluid flow inside a fracture
- No assumptions about geometry of the domain or fracture surface
- 3-D fracture interaction can capture near-wellbore tortuosity

References

- Savitski and Detournay, Propagation of a penny shaped fluid-driven fracture in an impermeable rock: asymptotic solutions, IJSS, 2002
- Gupta and Duarte, Coupled Formulation and Algorithms for Simulation of Non-Planar 3-D Hydraulic Fractures using the GFEM, Submitted

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